

## **MEMORANDUM**

W.O. 59822

TO:

Mr. Mark Kozak

Public Works Director

City of Kodiak

FROM:

Manager, Geotechnical Engineering

THROUGH: Aaron R. Christie, P.E.

Civil Engineer

DATE:

June 12, 2012

SUBJECT:

Downtown Water, Sewer, and Storm Drain Master Plan

Test Boring Investigation

## INTRODUCTION

Nine 15-foot-deep test borings were drilled in Center Street, Marine Way, Mission Road and Kashevarof Avenue on December 2, 4, and 5, 2011. The purpose of these borings was to determine the approximate depth to bedrock in support of the Downtown Water, Sewer, and Storm Drain Master Plan project.

Test borings were located in the field by taking swing tie measurements from existing features. The locations of the test borings are shown on the attached Figure A, Test Boring Location Map.

The test borings were drilled with a Mobile B-61 truck-mounted drill rig fitted with continuous flight, 8-inch diameter, hollow-stem auger. The rig is owned and operated by Denali Drilling, Inc., of Anchorage. The drilling was supervised and the samples logged by a civil engineer with our firm.

Disturbed samples were obtained at 2.5-foot intervals to a depth of 10 feet and one sample at a depth of 15 feet. The penetration test is performed by driving a 2.5-inch inside-diameter, split-spoon sampler a distance of 18 inches ahead of the auger with a 340-pound hammer falling 30 inches. The penetration resistance value shown on the test boring logs indicates the number of blows required to drive the sampler the last 12 inches. The values shown in the logs are raw data from the field and have not been adjusted for sampling equipment type or overburden pressure.

As the soil samples were recovered, they were visually classified and sealed in plastic bags to preserve the natural water content. The samples were then transported to DOWL HKM's laboratory in accordance with ASTM D4220, for further testing.

## **FINDINGS**

The depth to bedrock was difficult to determine while drilling the test borings. The bedrock is overlain with fill composed of gravel that looks the same as the samples taken in the weathered rock. Much of the rock could be drilled with the hollow stem auger and the weathered rock broke up during sampling to a sand and gravel. The test boring logs, attached as Figures 1 through 9, show our interpretation of the soil and rock. The depth to bedrock was estimated based on drill action, sample blow counts, observation of the recovered sample, correlation with bedrock outcrops, and previous excavations by Public Works. The results of particle size distribution tests performed on selected samples follow the boring logs.

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The bedrock in the study area is nearly vertically bedded and rock quality can change from soft, easily excavated rock to hard, unrippable rock in short horizontal distances. The surface of the bedrock is very irregular, so the depth to bedrock can also vary dramatically across short distances. This area of Kodiak has been extensively reworked over the years and some borings may have hit old utility excavations made into the rock and the rock surface could be much shallower a short distance away.

Test Boring 3 encountered a void between 8 and 10 feet below existing grade. It is assumed that this was an abandoned storm drain because the sampler suddenly encountered resistance at a depth of 8 feet and after 35 blows, broke through the obstruction and dropped two feet. The auger was retracted from the 7.5-foot depth and the rig moved about 3 feet away and the boring continued as Test Boring 4. The bedrock surface was interpreted to be at a depth of 14 feet in Test Boring 4. This is deeper than expected and may not be accurate.

Test Boring 5 encountered bedrock at a depth of about 15 feet. This is deeper than anticipated. The adjacent Kodiak National Wildlife Visitor Center building on the southeast corner of Center Street and Mission Road is founded on shallow bedrock and bedrock outcrops can be observed in the cut on the Marine Way side of the Wildlife Visitor Center and the Baranof Museum lot. Test Boring 6 in Marine Way encountered bedrock at a depth of about 13 feet. Although this boring location is near the bedrock outcrops, this boring is believed to accurately depict a steeply dipping bedrock surface.

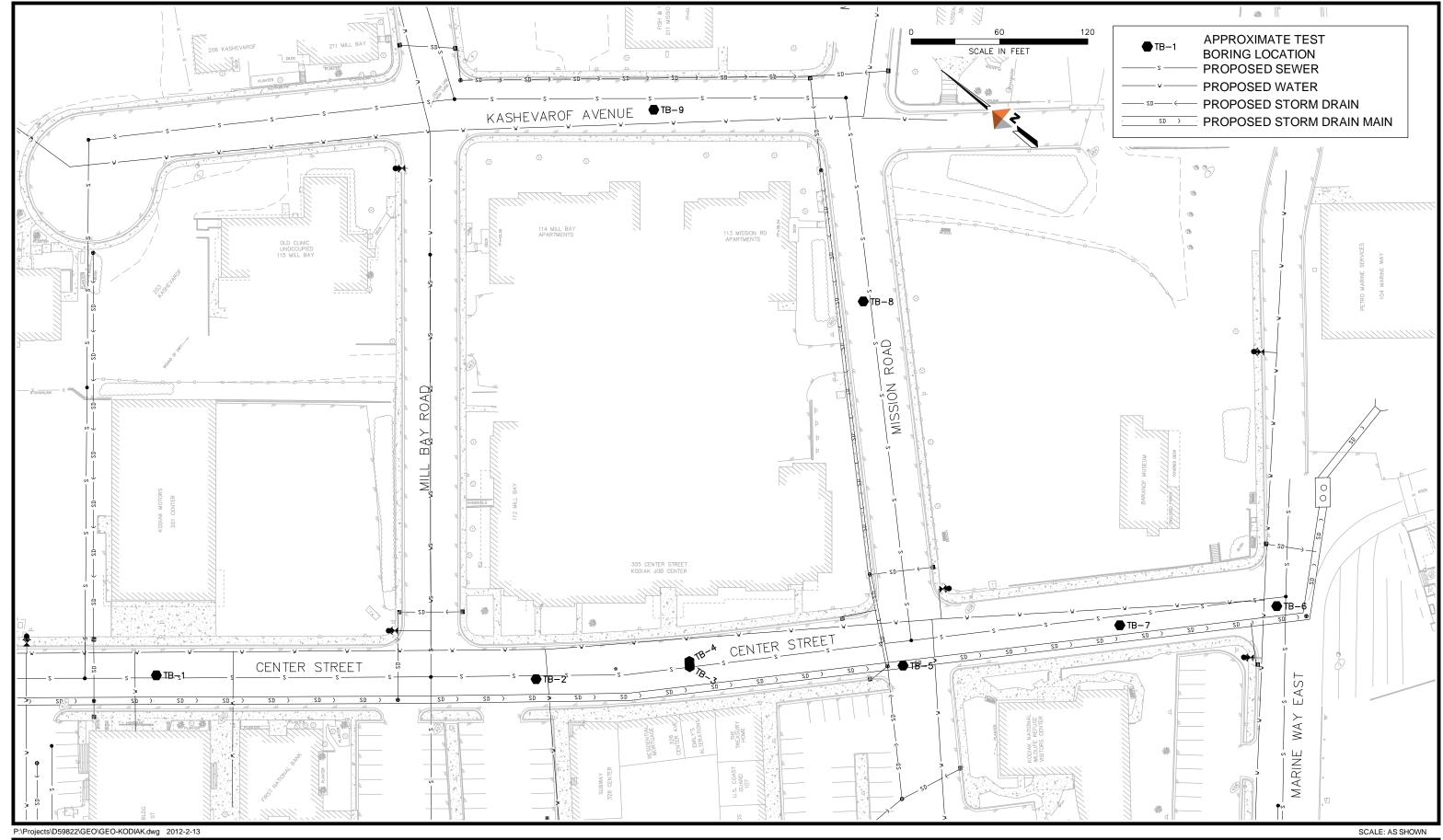
No environmental testing or monitoring was conducted as a part of this investigation. However, a hydrocarbon odor and sheen was noticed in Test Boring 4 below a depth of about 10 feet.

## ENGINEERING ANALYSIS AND RECOMMENDATIONS

The bedrock penetrated with the hollow stem auger can be excavated with considerably more effort than required to excavate dense gravel. There are likely to be near vertical layers within the bedrock formation that cannot be excavated without the use of a large hydraulic hammer to fracture the rock. Blasting is not desirable considering the close proximity of utilities and structures. Should blasting be required, it should be performed in conformance with the City of Kodiak Standard Construction Specifications.

The construction contractor should expect a large backhoe equipped with a rock bucket and a large hydraulic hammer will be required for any rock excavation.

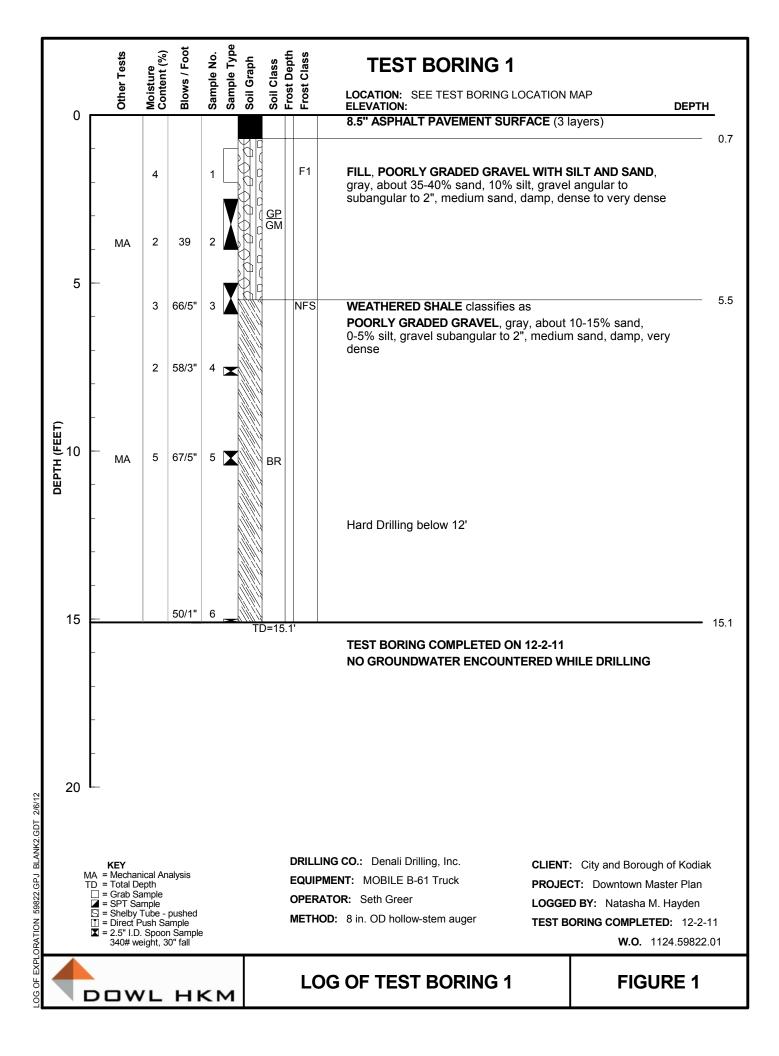
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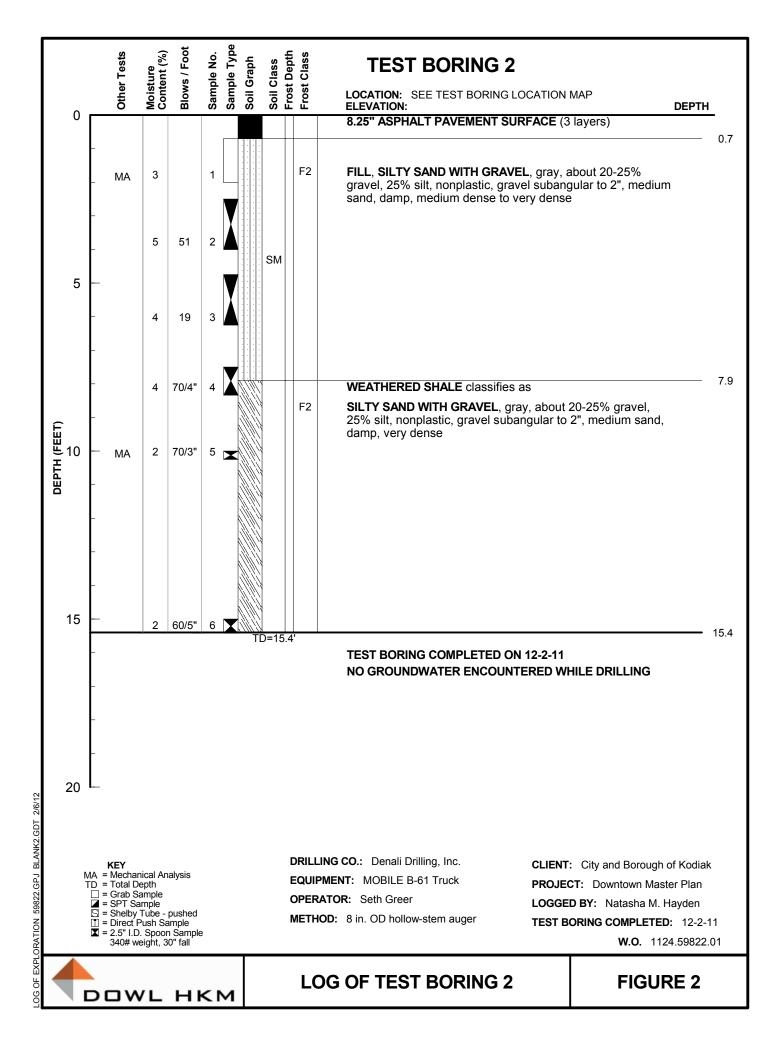


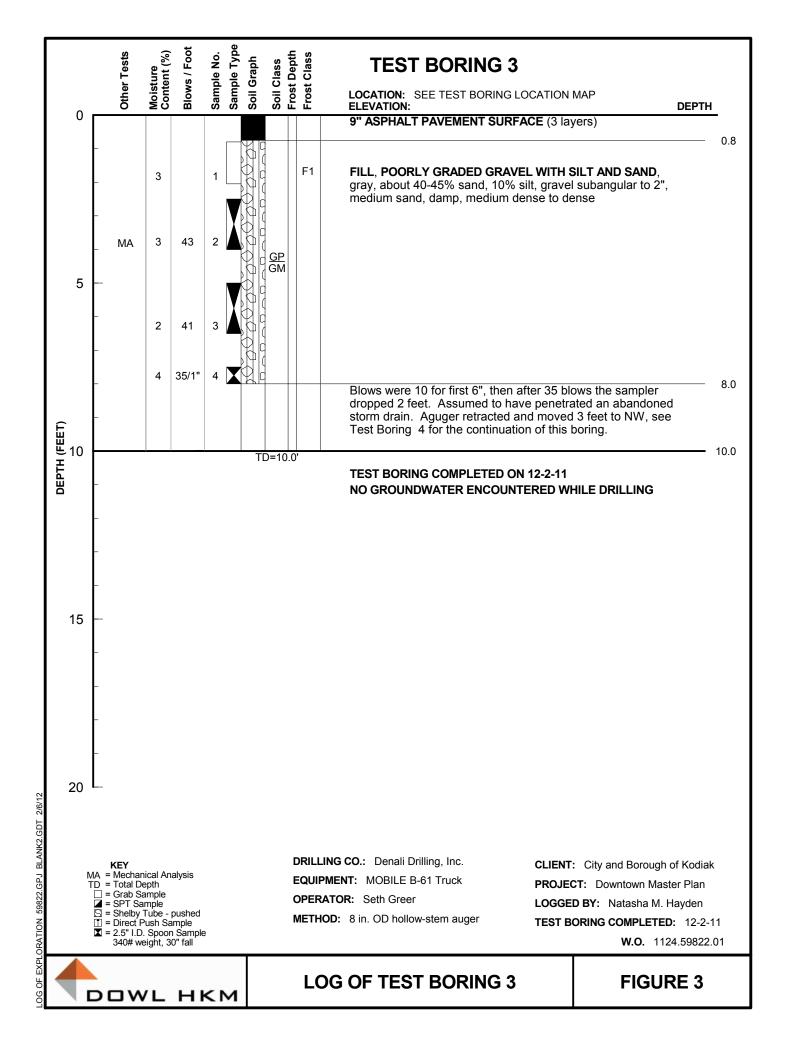
DOWL HKM

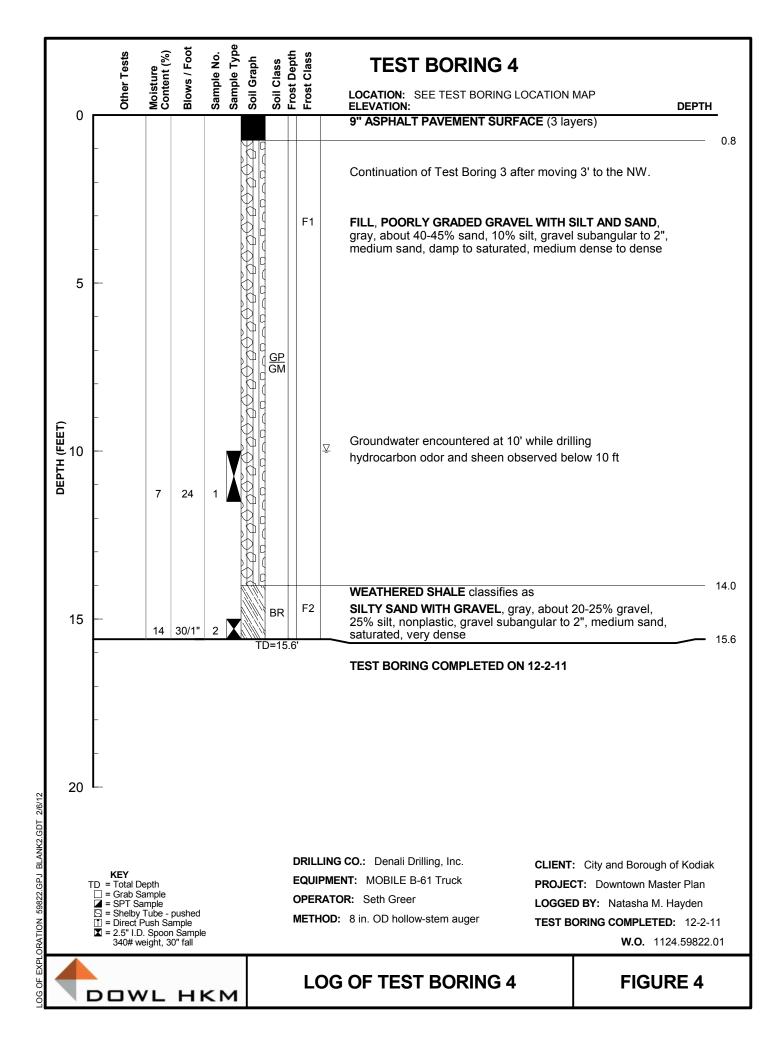
Test Boring Location Map DOWNTOWN WATER, SEWER, AND STORM DRAIN MASTER PLAN Kodiak, Alaska

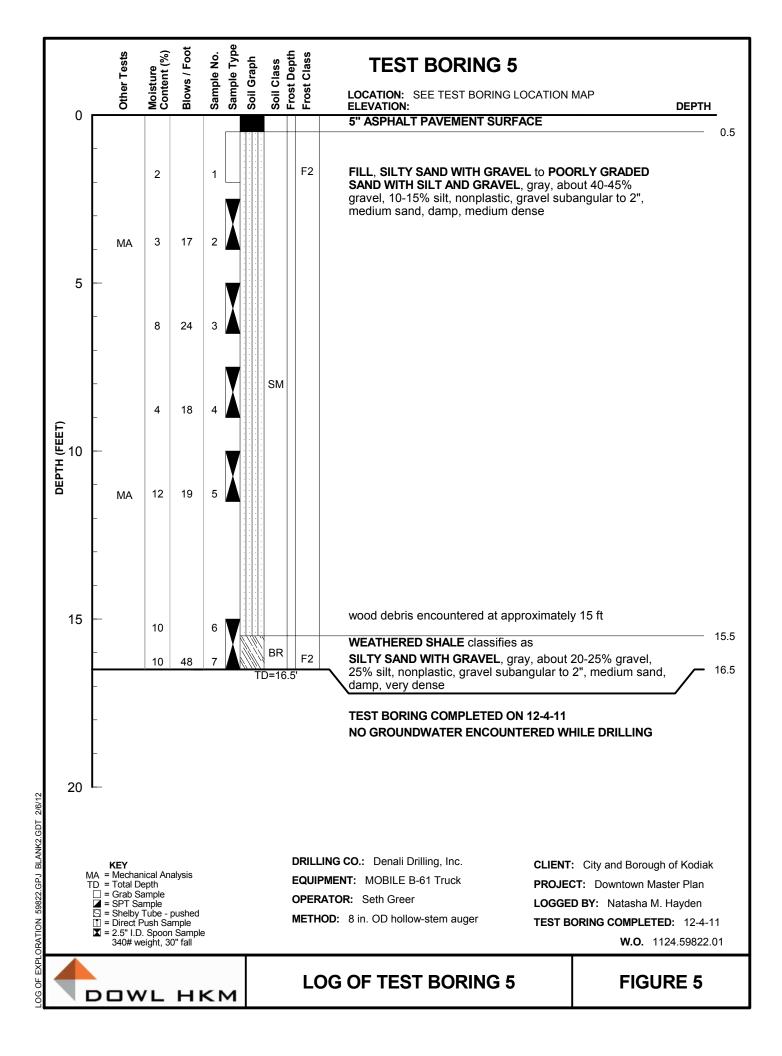
FIGURE A

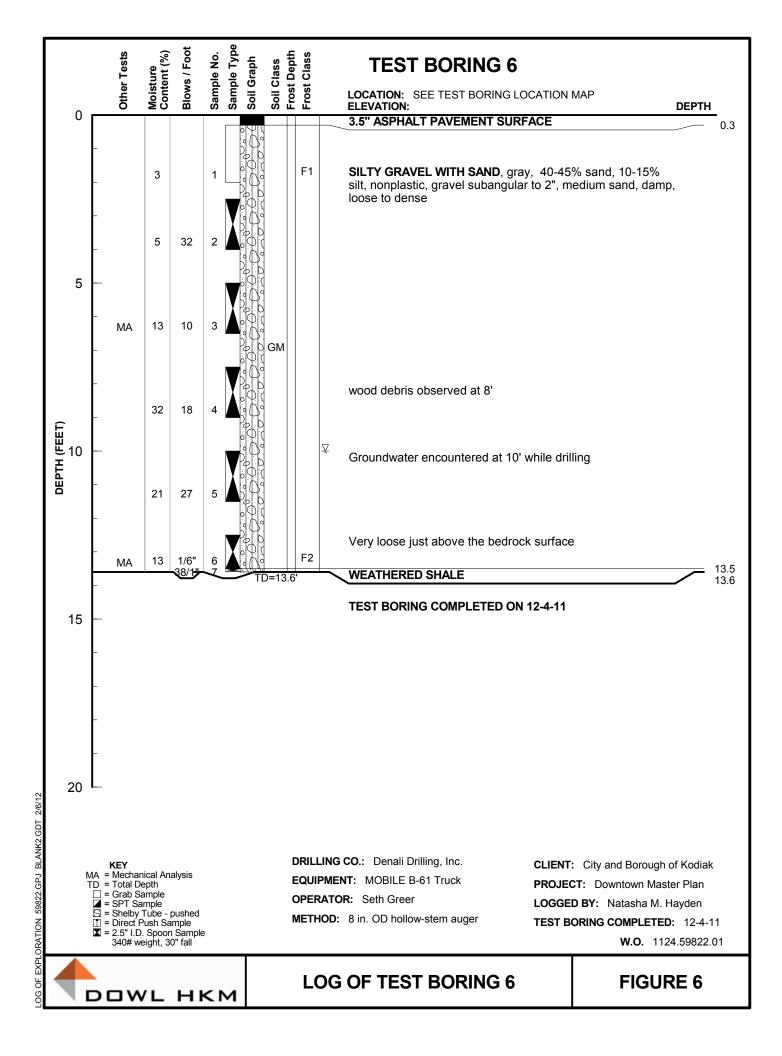


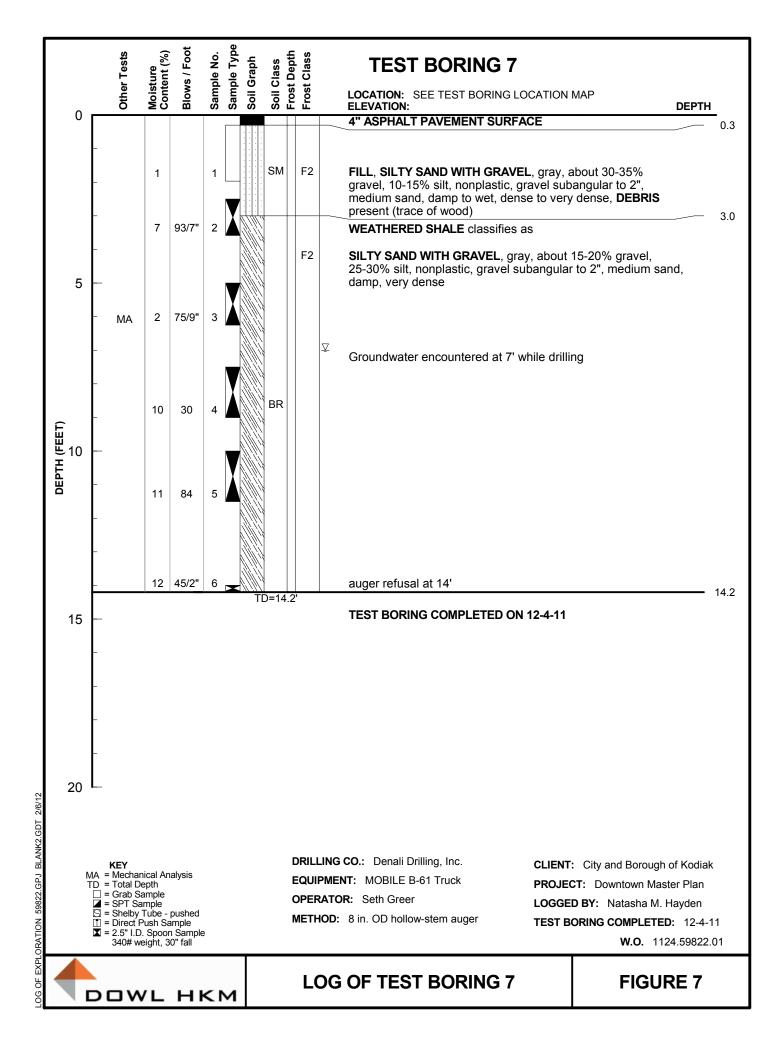


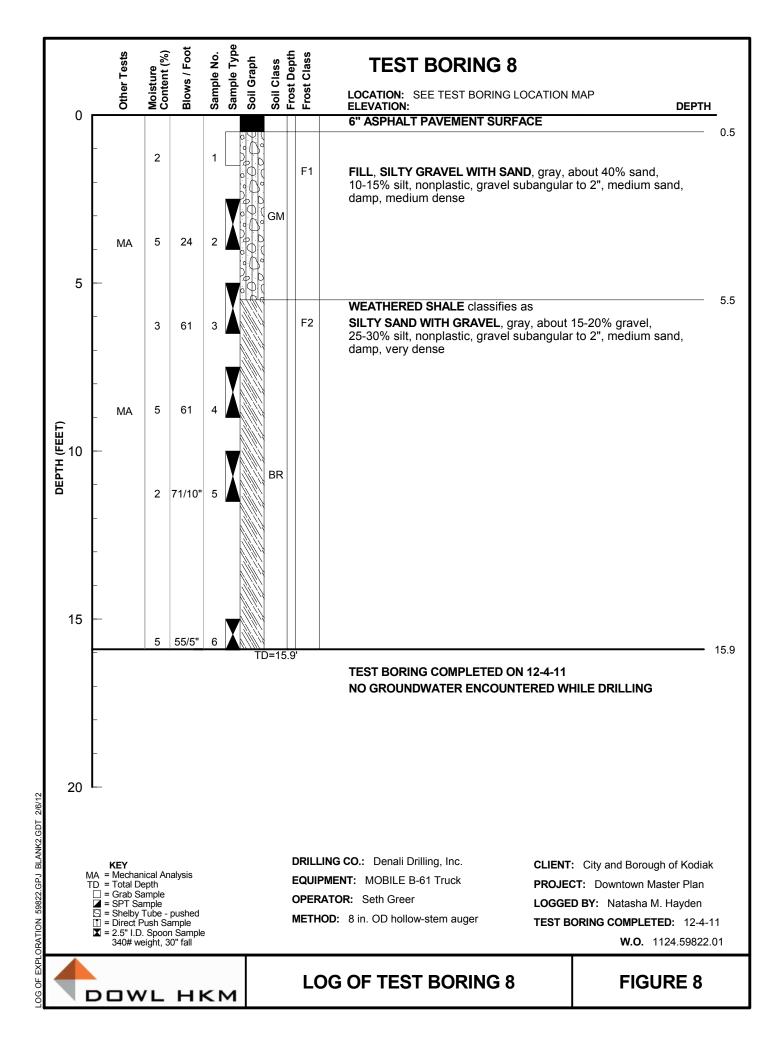


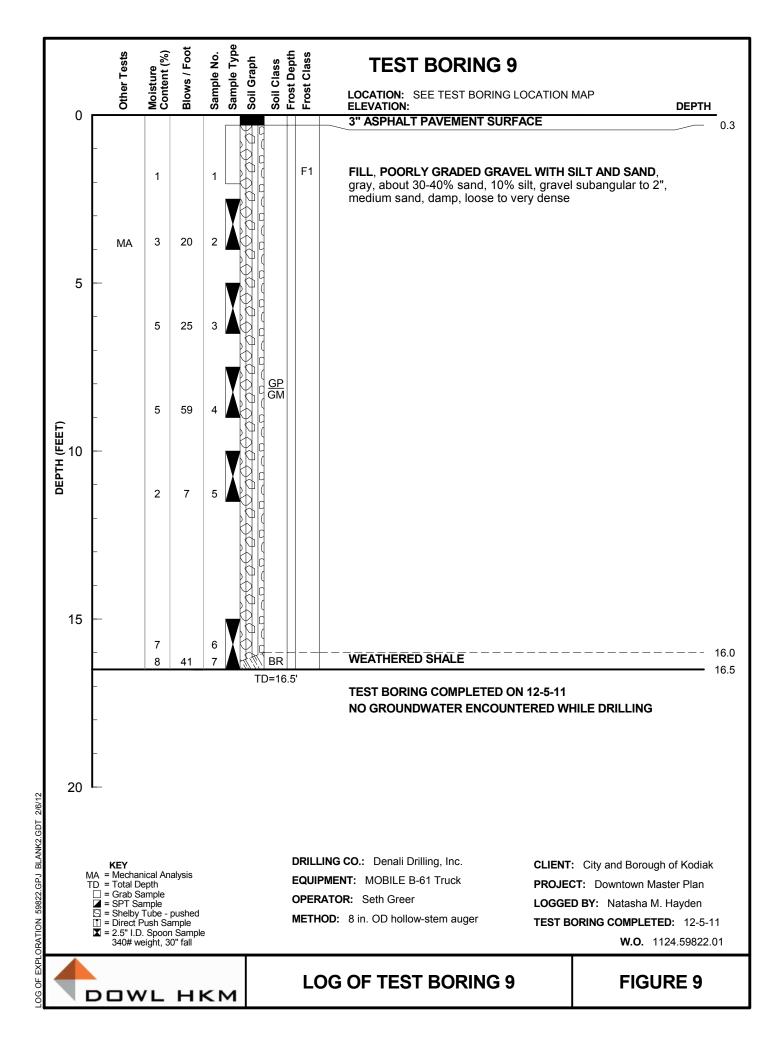












## **TEST BORING LOG - DESCRIPTIVE GUIDE**

<u>Soil Descriptions</u> - The soil is classified visually in the field based on drill action, auger cuttings, and sample information. The recovered soil samples are classified visually again in the laboratory. The soil description on the boring log is based on an interpretation of the field and laboratory visual classifications, along with the results of laboratory particle-size distribution analyses and Atterberg Limits tests which may have been performed.

The <u>soil classification</u> is based on ASTM Designation D2487 "Standard Test Method for Classification of Soils for Engineering Purposes" and ASTM D2488 "Standard Practice for Description and Identification of Soils (Visual - Manual Procedure)". The <u>soil frost classification</u> is based on the system developed by the U.S. Army Corps of Engineers and is performed in accordance with the Departments of the Army and Air Force Publication TM 5-822-5 "Pavement Design for Roads, Streets, Walks, and Open Storage Areas". Outlines of these classification procedures are presented on the following pages.

The soil color is the subjective interpretation of the individual logging the test boring.

The <u>plasticity</u> of the minus No. 40 fraction of the soil is described and the fine-grained soils are identified from manual tests using the following table as a guide:

Soil Symbol	Dry Strength	Dilatancy	Toughness
ML	none to low	slow to rapid	low or thread cannot be formed
CL	medium to high	none to slow	medium
MH	low to medium	none to slow	low to medium
CH	high to very high	none	high

Plasticity Description	Criteria
Nonplastic	A 1/8" (3.2mm) thread cannot be rolled at any water content.
Low	A thread can barely be rolled and the lump cannot be formed when drier than the plastic limit.
Medium	The thread is easy to roll and not much time is required to reach the plastic limit. The thread cannot be rerolled after reaching the plastic limit. The lump crumbles when drier than the plastic limit.
High	It takes considerable time rolling and kneading to reach the plastic limit. The thread can be rerolled several times after reaching the plastic limit. The lump can be formed without crumbling when drier than the plastic limit.

Laboratory Atterberg Limits tests usually are performed on a few of the plastic soils and results are reported on the test boring log. These laboratory tests are performed in accordance with ASTM D4318 "Standard Test Method for Liquid Limit, Plastic Limit, and Plasticity Index of Soils."

The shape of the gravel particles is described based on this guide:

Angular: particles have sharp edges and relatively plane sides with unpolished

surfaces.

Subangular: particles are similar to angular but have somewhat rounded edges.

Subrounded: particles exhibit nearly plane sides but have well-rounded corners and

edges.

Rounded: particles have smoothly curved sides and no edges.

The <u>size of gravel and sand particles</u> is described using this guide:

	Gravel	Sand
Coarse:	Passes 3" (75 mm) sieve, retained on 3/4" (19 mm) sieve	Passes No. 4 sieve, retained on No. 10 sieve
Medium:	N/A	Passes No. 10 sieve, retained on No. 40 sieve
Fine:	Passes 3/4" (19 mm) sieve, retained on No. 4 sieve	Passes No. 40 sieve, retained on No. 200 sieve

The soil moisture is described as:

dry: powdery, dusty, no visible moisture.

damp: enough moisture to affect the color of the soil; moist.

wet: water in pores but not dripping; capillary zone above water table.

saturated: dripping wet, contains significant free water, or sampled below water

table.

The subjective estimate of the <u>density of coarse-grained soils</u> is based on the observed drill action and on drive sample data. The guide below is used for sands with minor amounts of fine gravel; however, blowcounts can be affected strongly by gravel content, thermal state, drilling procedures, condition of equipment and performance of the test.

Standard Penetration Resistance N (blows / foot) or N (blows / 300 mm)	Soil Density
0 - 5	Very loose
6 - 10	Loose
11 - 30	Medium dense
31 - 50	Dense
More than 50	Very dense

An estimate of the <u>consistency of fine-grained soils</u> is based on the observed drill action and on drive sample data. The guide below is used:

Standard Penetration Resistance N (blows / foot) or N (blows / 300 mm)	Soil Consistency
0 - 2 3 - 4	Very soft Soft
3 - 4 5 - 8	Sott Firm
9 - 15	Stiff
15 - 30	Very stiff
More than 30	Hard

<u>Soil Layer Boundaries</u> - Generally, there is a gradual transition from one soil type to another in a natural soil deposit, and it is difficult to determine accurately the boundaries of the soil layers.

- A diagonal line between soil layers on the graphic boring log indicates the general region of transition from one soil layer to another.
- A dashed diagonal line indicates the soil boundary was detected only by a change in the recovered samples and the actual boundary may be anywhere between the indicated sample depths.
- A horizontal line between soil layers indicates a relatively distinct transition between soil types was observed in the recovered samples and / or by a distinct change in drill action.

<u>Sample Interval</u> - The sample interval is shown graphically on the test boring log and generally is accurate to about 0.5 foot (0.15 meter).

<u>Frost Depth and Soil Temperatures</u> - If frozen ground is encountered during drilling, the interval of frozen soil is shown graphically on the test boring log. Generally, the temperature of a few soil samples is measured and shown on the boring log. These sample temperatures only give a qualitative indication of the *in situ* soil temperatures. The temperature of samples can be influenced significantly by the ambient air temperature and friction during drilling and sampling.

<u>Soil Moisture Content</u> - Generally, laboratory soil moisture content tests are performed on all recovered samples. Only about 30 grams of the minus No. 4 material typically is used for the moisture content test, so results reported on the log may not reflect accurately the *in situ* moisture content of gravelly soils.

<u>Soil Density</u> - The soil density shown on the test boring logs generally is determined by measuring the wet weight, moisture content, and physical dimensions of relatively undisturbed specimens.

<u>Ground Water</u> - The depth to ground water observed during drilling generally is shown on the test boring log. The depth to ground water observed during drilling can differ significantly from the depth to the actual ground water table, particularly in fine-grained soils. When more accurate water level measurements are desired, we typically install perforated PVC pipe in a boring to monitor the ground water level.

<u>Penetration Resistance, N</u> - Standard penetration tests (SPT) are performed in accordance with ASTM Designation D1586 "Standard Method for Penetration Test and Split-Barrel Sampling of Soils." A modified penetration test using a 2.5-inch (63.5 mm) I.D. split spoon driven with a 340-pound (154.2 kg) hammer falling 30 inches (.76 m) is performed to obtain larger samples, particularly in gravelly soils. The boring log key describes the graphic symbols used to differentiate between sample types.

<u>Undisturbed Samples</u> - Undisturbed Shelby tube samples are obtained in accordance with ASTM Designation D1587, "Standard Practice for Thin-Walled Tube Sampling of Soils." Generally, 3-inch (76.2 mm) O.D. Shelby tubes are used. Relatively undisturbed liner samples are obtained in accordance with ASTM Designation D3550, "Standard Practice for Ring-Lined Barrel Sampling of Soils," except a thick-walled cutting shoe is used. Typically, the sampler is driven using a 340-pound (154.2 kg) weight falling 30 inches (.76 m). The typical brass liner has an I.D. of 2.4 inches (91 mm).

<u>Grab Samples</u> - Grab samples are obtained from the auger flights. The sample depth and interval indicated on the test boring log should be considered a rough approximation. The grab samples may not be representative of *in situ* soils, particularly in layered soil deposits.

Soil Classification

## CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES ASTM DESIGNATION: D2487 Based on the Unified Soil Classification System

			•		
	Criteria for Assigning Group Symbols and Group Names Using Laboratory $\operatorname{Tests}^A$	ools and Group Names Using Lab	ooratory Tests <sup>A</sup>	Group Symbol	Group Name <sup>B</sup>
Coarse-Grained Soils	Gravels	Clean Gravels	$Cu \ge 4$ and $1 \le Cc \le 3^E$	GW	Well-graded gravel <sup>F</sup>
More than 50% retained on #200 sieve	More than 50% of coarse fraction retained on #4 sieve	Less than 5% fines $^{\mathcal{C}}$	$Cu < 4$ and/or $1 > Cc > 3^E$	GP	Poorly graded gravel <sup>F</sup>
		Gravel with Fines	Fines classify as ML or MH	GM	Silty gravel F,G,H
		More than 12% fines <sup>C</sup>	Fines classify as CL or CH	CC	Clayey gravel F, G, H
	Sands	Clean Sands	$Cu \ge 6$ and $1 \le Cc \le 3^E$	ΜS	Well-graded sand1
	50% or more of coarse fraction passes #4 sieve	Less than 5% fines <sup>D</sup>	$Cu < 6$ and/or $1 > Cc > 3^E$	SP	Poorly graded sand <sup>I</sup>
	•	Sands with Fines	Fines classify as ML or MH	SM	Silty Sand G,H,I
		More than 12% fines <sup>D</sup>	Fines classify as CL or CH	SC	Clayey Sand G,H,I
Fine-Grained Soils	Silts and Clays	Inorganic	PI > 7 and plots on or above "A" line	CL	Lean Clay K.L.M
50% or more passes the	Liquid limit less than 50		PI < 4 or plots below "A" Line J	ML	Silt <sup>K,L,M</sup>
#200 sieve		Organic	Liquid limit - oven dried <0.75	ТО	Organic Clay K,L,M,N
			Liquid limit - not dried	70	Organic silt K,L,M,O
	Silts and Clays	Inorganic	PI plots on or above "A" line	СН	Fat clay K,L,M
	Liquid limit 50 or more		PI plots below "A" line	MH	Elastic silt K,L,M
		Organic	Liquid limit - oven dried <0.75	НО	Organic clay <sup>K,L,M,P</sup>
			Liquid limit - not dried	НО	Organic clay <sup>K,L,M,Q</sup>
Highly organic soils		Primarily organic matter,	dark in color, and organic odor	PT	Peat

A Based on the material passing the 3-in. (75nm) sieve.	SP-SC poorly graded sand with clay	M If soil contains $\geq$ 30% plus No. 200, predominantly gravel, add "gravelly" to
B If field sample contained cobbles or boulders, or both, add "with cobbles or	E Cu = D200 Ce = D200 <sup>2</sup>	group name.
boulders, or both" to group name.	D <sub>10</sub> D10 <sup>xD</sup> 60	N PI $\geq$ 4 and plots on or above "A" line.
С Gravels with 5 to 12% fines require dual symbols:	F If soil contains > 15% sand, add "with sand" to group name.	O PI < 4 or plots below "A" line.
GW-GM well-graded gravel with silt	G If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.	P PI plots on or above "A" line.
GW-GC well-graded gravel with clay	H If fines are organic, add "with organic fines" to group name.	Q PI plots below "A" line.
GP-GM poorly graded gravel with silt	I f soil contains > 15% gravel, add "with gravel" to group name.	
GP-GC poorly graded gravel with clay	J If Atterberg Limits plot in hatched area, soil is a CL-ML, sifty clay.	
D Sands with 5 to 12% fines require dual symbols:	K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel",	
SW-SM well-graded sand with silt	whichever is predominant.	
SW-SC well-graded sand with clay	L If soil contains $\geq$ 30% plus No. 200, predominantly sand, add "sandy" to	
SP-SM poorly graded sand with silt	group name.	

# DESCRIPTION OF FROZEN SOILS (Visual-Manual Procedure) ASTM Designation: D4083

F	ମ	ì	ෆි	, {	f	ර		6	r	60		6		¥	7
Classify Soil Phase by ASTM D2487 or D2488	Field Identification	Identify by visual examination. To determine presence	of excess ice, use procedures under Note 2 and hand magnifying lens as necessary. For soils not fully satu-	rated, estimate degree of ice saturation; medium, low.	larger particles.	se, record	ion SS	Spacing Hardness Pattern of arrangement		Estimate volume of visible segregated for present as percentage of total sample volume.	Designate material as ICE (Note 3) and use descriptive terms as follows, usually one item from each group,	pplicable: <u>less</u>	CLOOD I CLOOD I [of mass, not individual POROUS crystals] GRANULAR STRATIFIED	Color (Examples):	COLORLESS Admixtures (Examples) GRAY CONTAINS FEW THIN BLUE SILT INCLUSIONS
Phase by ASTN		Symbol	Ŋ	N <sub>b</sub> N <sub>bn</sub>	Nbe	××	°	٧	Vs	$V_{\mathbf{u}}$	ICE + Soil Type		ICE		
Classify Soil	GnorgduS	Description	Poorly bonded or friable	No excess ice Well-bonded	Excess ice	Individual ice crystal or inclusions	Ice coatings on particles	Random or irregularly oriented ice formations	Stratified or distinctly oriented ice formations	Uniformly distributed ice	Ice with soil inclusions		Ice without soil inclusions		
	Group	Symbol	Z				>						ICE		
			Segregated ice is not	visible by	2	Segregated	ice is visible by eye (ice 1-inch	(25 mm) or less in thickness)				Ice (greater	tnan I-inch (25 mm) in thickness)		:
Part I Description of Soil Phase					Part II Description of	Frozen Soil						Part III	Description of Substantial Ice		

- Frozen soils in the N group may, on close examination, indicate presence of ice within the voids of the material by crystalline reflections or by a sheen on fractured or trimmed surfaces. The impression received by the unaided eye, however, is that none of the frazen water occupies space in excess of the original voids in the soil. The opposite is true of frozen soils in the V group. Note 1:
- When visual methods may be inadequate, a simple field test to aid in evaluation of the volume of excess ice can be made by placing some frozen soil in a small jar, allowing it to melt, and observing the quantity of supernatant water as a percentage of total volume. Note 2:
  - Where special forms of ice such as hoarfrost can be distinguished, more explicit description should be given. Note 3:
    - Note 4: Observer should be careful to avoid being misled by surface scratches or frost coating on the ice.

## DEFINITIONS

- ice coetings on Parides discernible layers of ice found on or below the larger soil particles in a frozen soil mess.
- log Crystal a very small individual ice particle visible in the face of a soil mass. Crystals may be present alone or in combination with other ice formations.
- Clear loe ice that is transparent and contains only a moderate number of air bubbles.
- Cloudy log ice that is translucent or relatively opeque due to the content of air or for other reasons, but which is essentially sound and impervious.
- 5) Poous leg ice that contains numerous voids, usually interconnected and usually resulting from meiting at air bubbles or along crystal interfaces from presence of salt or other materials in the water, or from the freezing of saturated snow. Though poous, the mass retains its structural unity.
- 6) Canded log ice that has rotted or otherwise formed into long columnar crystals, very loosely bonded together.
- Granufar log ice that is composed of coarse, more or less equidimensional crystals weakly bonded trgether.
- 8) <u>loe Lensss</u>-entrodaries formations in soil occurring essentially parallel to each other, generally normal to the direction of heat loss, and commonly in repeated layers.
- 9) lea Segregation the growth of ice within soil in excess of the amount that may be produced by the in-place conversion of the original void moisture to ice. Ice segregation occurs most often as distinct lenses, layers, veins, and masses, commonly, but not always, oriented normal to the direction of heat
- 10) Wel-Bondeg a condition in which the sol particles are strongly held together by the ice so that the frozen sol possesses relatively high resistance to chipping or breaking.
- Poork-Bonded a condition in which the soil particles are weakly held together by the ice so that the frozen soil has poor resistance to chipping and breaking.
- 12) Thew Stable the characteristics of frozen soils that, upon trawing, do not show loss of strength in comparison b normal, long-time trawed values not produce detrimental settlement.

## FROST DESIGN SOIL CLASSIFICATION<sup>1</sup>

	Percentage Finer than 0.02	Typical Soil Types Under Unified Soil Classification
	mm by Weight	System
(a) Gravels	0 to 1.5	GW and GP
(b) Sands	0 to 3	SW and SP
(a) Gravels	1.5 to 3	GW and GP
Clustica fock		
(b) Sands	3 to 10	SW and SP
Gravelly soils	3 to 6	GW, GP, GW-GM, and GP-GM
Sandy soils	3 to 6	SW, SP, SW-SM, and SP-SM
Gravelly soils	6 to 10	GM, GW-GM, and GP-GM
(a) Gravelly soils	10 to 20	GM, GW-GM, and GP-GM
(b) Sands	6 to 15	SM, SW-SM, and SP-SM
(a) Gravelly soils	Over 20	GM and GC
(b) Sands, except very fine silty sands	Over 15	SM and SC
(c) Clays, PI>12		CL and CH
(a) All silts		ML and MH
(b) Very fine silty sands	Over 15	SM
(c) Clays, PI<12		CL and CL-ML
(d) Varved clays and		CL and ML
other fine-grained,		CL, ML, and SM
banded sediments		CL, CH, and ML CL, CH, ML and SM
	Crushed stone Crushed rock  (b) Sands  (a) Gravels Crushed stone Crushed rock  (b) Sands  Gravelly soils  Sandy soils  Gravelly soils  (a) Gravelly soils  (b) Sands  (a) Gravelly soils  (b) Sands  (c) Clays, PI>12  (a) All silts  (b) Very fine silty sands  (c) Clays, PI<12  (d) Varved clays and	(a) Gravels Crushed stone Crushed rock  (b) Sands  (a) Gravels Crushed stone Crushed rock  (b) Sands  (c) Crushed stone Crushed rock  (d) Sands  (e) Crushed stone Crushed stone Crushed rock  (f) Sands  (g) Gravelly soils  (g) Gravelly soils  (h) Sands  (h) Cravelly soils  (h) Cravelly soil

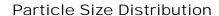
<sup>&</sup>lt;sup>1</sup> Departments of the Army and Air Force Publication TM 5-822-5/AFM 88-7, "Pavement Design for Roads, Streets, Walks, and Open Storage Areas", Table 18-2.

<sup>2</sup> Corps of Engineers Frost groups directly correspond to the Municipality of Anchorage soil frost classification groups,

except as noted.

Non Frost-Susceptible.

Possibly frost-susceptible, but requires laboratory test to determine frost design soil classification.





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1869

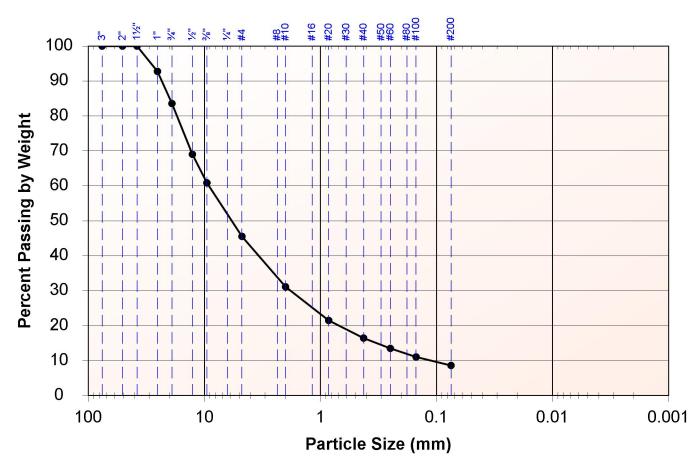
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**Reported** 12/15/2011

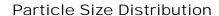
Location: Test Boring 1

Sample 2 Depth 2.5'-4'

Engineering Classification: Poorly Graded Gravel with Silt and Sand, GP-GM



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	93%	
3/4"	84%	
1/2"	69%	
Ä	61%	
#4	46%	
Total Wei	ght of Coarse Fr	action: 591.9g
#10	31%	
#20	21%	
#40	16%	
#60	13%	
#100	11%	
#200	8.6%	
Total Wei	ght of Fine Fract	ion: 269.2g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2010-1870

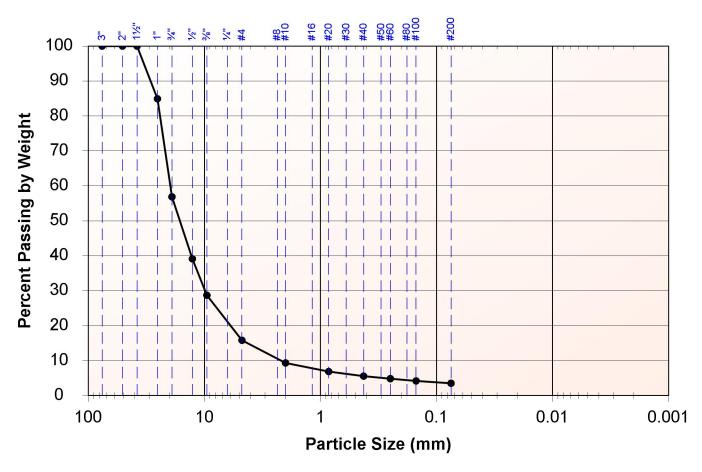
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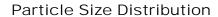
Location: Test Boring 1

Sample 5 Depth 10'-11.5'

**Engineering Classification: Well Graded Gravel, GW** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	85%	
3/4"	57%	
1/2"	39%	
Ä	29%	
#4	16%	
Total Weig	ht of Coarse Fra	action: 357.9g
#10	9%	
#20	7%	
#40	6%	
#60	5%	
#100	4%	
#200	3.5%	
Total Weig	tht of Fine Fract	ion: 56.6g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1871

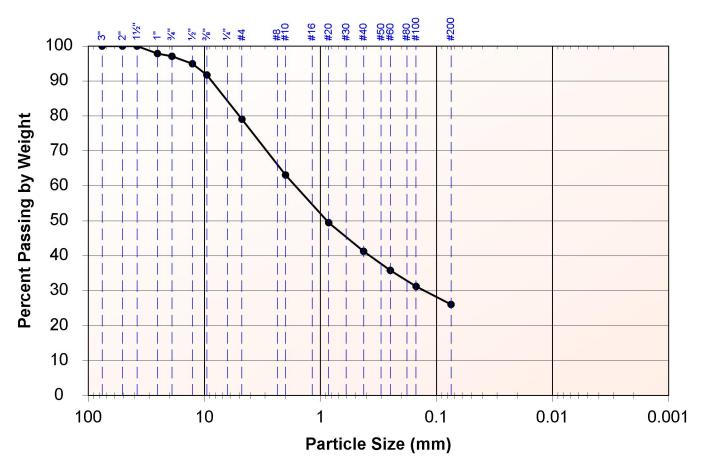
**Received** 12/4/2011

**Reported** 12/15/2011

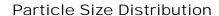
**Location:** Test Boring 2

Sample 1 Depth 0'-2'

**Engineering Classification: Silty Sand with Gravel, SM** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	98%	
3/4"	97%	
1/2"	95%	
Ä	92%	
#4	79%	
Total Weig	ght of Coarse Fra	action: 3681.7g
#10	63%	
#20	49%	
#40	41%	
#60	36%	
#100	31%	
#200	26.1%	
Total Weig	ght of Fine Fract	ion: 353.2g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1872

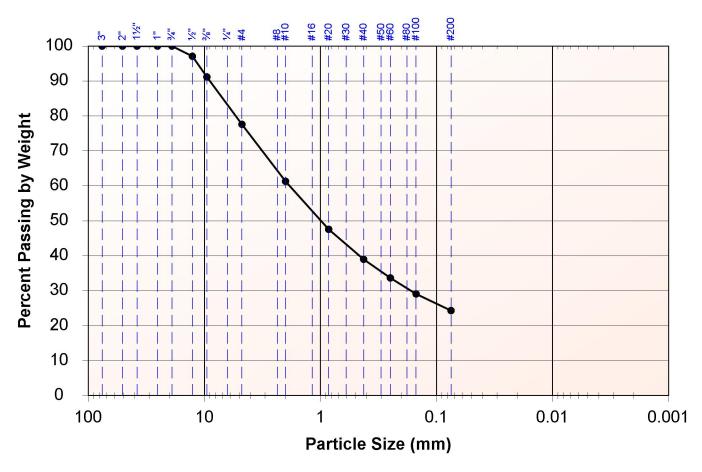
**Received** 12/4/2011

**Reported** 12/15/2011

**Location:** Test Boring 2

Sample 5 Depth 10'-11.5'

**Engineering Classification: Silty Sand with Gravel, SM** 



Size	Passing	Specification
3"	100%	Opecinication
2"	100%	
1½"	100%	
1"	100%	
3/4"	100%	
/4 1/2"	97%	
Ä	91%	
#4	78%	
		440F O
	ght of Coarse Fra	action: 1105.9g
#10	61%	
#20	48%	
#40	39%	
#60	34%	
#100	29%	
#200	24.3%	
Total Weig	ght of Fine Fracti	ion: 350.4g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1873

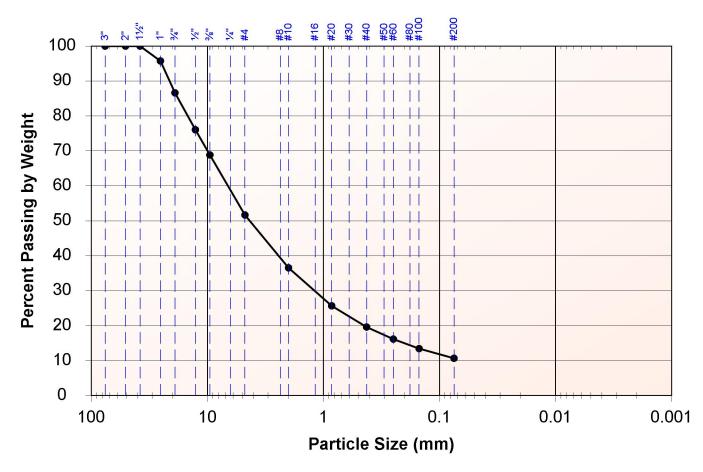
**Received** 12/4/2011

**Reported** 2/3/2012

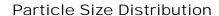
**Location:** Test Boring 3

Sample 2 Depth 2.5'-4'

Engineering Classification: Poorly Graded Gravel with Silt and Sand, GP-GM



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	96%	
3/4"	87%	
1/2"	76%	
Ä	69%	
#4	52%	
Total Wei	ght of Coarse Fra	action: 1601.7g
#10	37%	
#20	26%	
#40	20%	
#60	16%	
#100	13%	
#200	10.7%	
Total Wei	ght of Fine Fracti	ion: 301.2g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1874

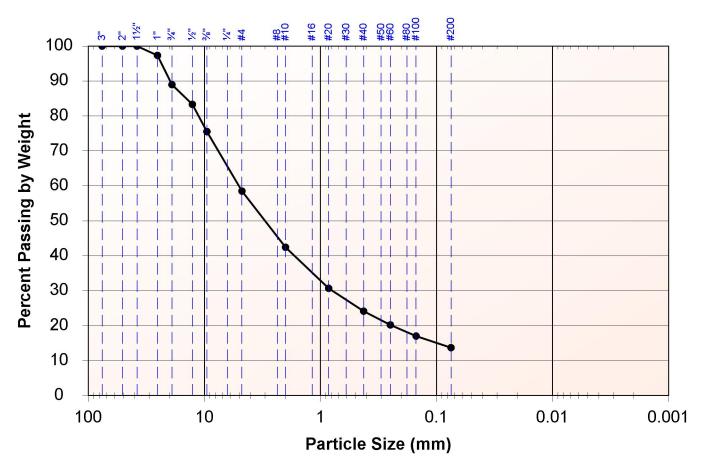
**Received** 12/4/2011

**Reported** 12/15/2011

**Location:** Test Boring 5

Sample 2 Depth 2.5'-4'

**Engineering Classification: Silty Sand with Gravel, SM** 



Size	Passing	Specification
3"	100%	•
2"	100%	
1½"	100%	
1"	97%	
3/4"	89%	
1/2"	83%	
Ä	76%	
#4	59%	
Total Wei	ght of Coarse Fr	action: 1492.2g
#10	42%	
#20	31%	
#40	24%	
#60	20%	
#100	17%	
#200	13.7%	
Total Wei	ght of Fine Fract	ion: 304.5g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1875

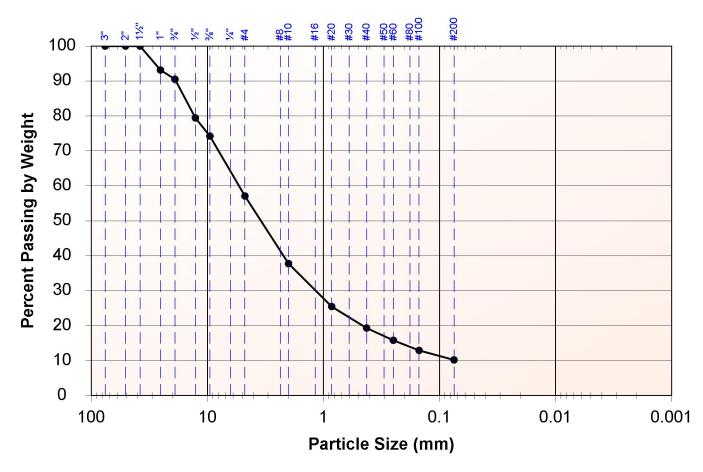
**Received** 12/4/2011

**Reported** 12/15/2011

**Location:** Test Boring 5

Sample 5 Depth 10'-11.5'

Engineering Classification: Poorly Graded Sand with Silt and Gravel, SP-SM



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	93%	
3/4"	91%	
1/2"	79%	
Ä	74%	
#4	57%	
Total Wei	ght of Coarse Fr	action: 2110.0g
#10	38%	
#20	25%	
#40	19%	
#60	16%	
#100	13%	
#200	10.2%	
Total Wei	ght of Fine Fract	ion: 377.3g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1876

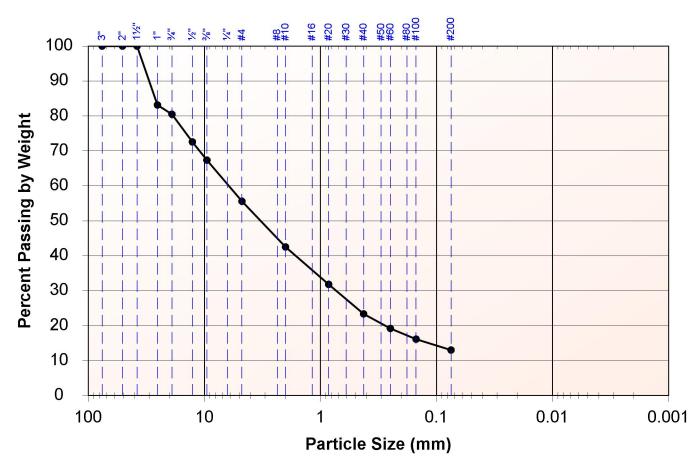
**Received** 12/4/2011

**Reported** 12/15/2011

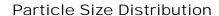
**Location:** Test Boring 6

Sample 3 Depth 5'-6.5'

**Engineering Classification: Silty Gravel with Sand, GM** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	83%	
3/4"	80%	
1/2"	73%	
Ä	67%	
#4	56%	
Total Wei	ght of Coarse Fra	action: 953.3g
#10	43%	
#20	32%	
#40	23%	
#60	19%	
#100	16%	
#200	13%	
Total Wei	ght of Fine Fracti	ion: 302.2g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1877

**Received** 12/4/2011

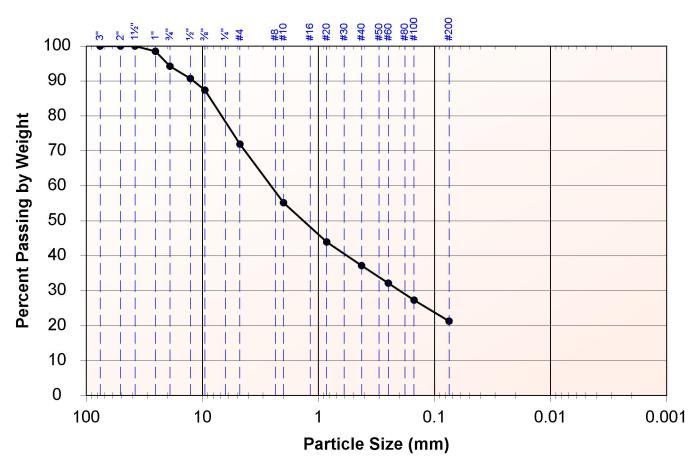
**Reported** 12/15/2011

**Location:** Test Boring 6

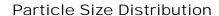
Sample 6

Depth 12.5'-13.5'

**Engineering Classification: Silty Sand with Gravel, SM** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	98%	
3/4"	94%	
1/2"	91%	
Ä	87%	
#4	72%	
Total Wei	ght of Coarse Fr	action: 1886.5g
#10	55%	
#20	44%	
#40	37%	
#60	32%	
#100	27%	
#200	21.3%	
Total Wei	ght of Fine Fract	ion: 353g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1878

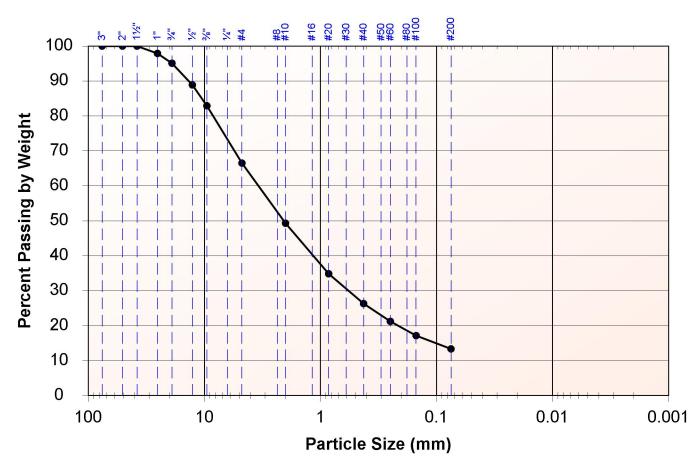
**Received** 12/4/2011

**Reported** 12/15/2011

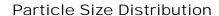
**Location:** Test Boring 7

Sample 3 Depth 5'-6.1'

**Engineering Classification: Silty Sand with Gravel, SM** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	98%	
3/4"	95%	
1/2"	89%	
Ä	83%	
#4	67%	
Total Weig	ght of Coarse Fr	action: 1188.9g
#10	49%	
#20	35%	
#40	26%	
#60	21%	
#100	17%	
#200	13.4%	
Total Weig	ght of Fine Fract	ion: 389.5g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1880

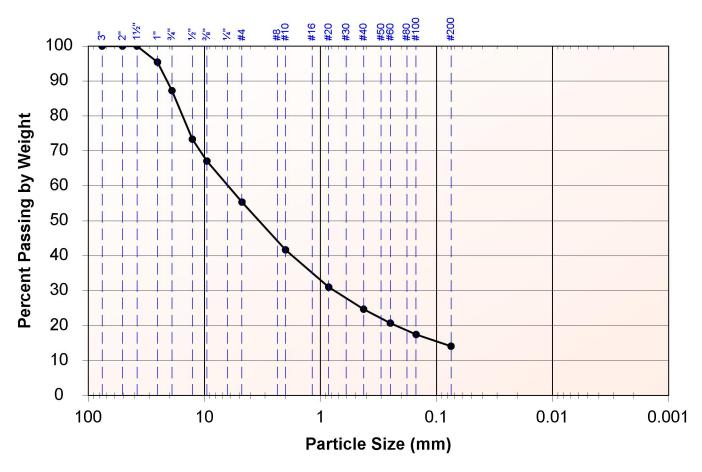
**Received** 12/4/2011

**Reported** 12/15/2011

**Location:** Test Boring 8

Sample 2 Depth 2.5'-4'

**Engineering Classification: Silty Gravel with Sand, GM** 



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	95%	
3/4"	87%	
1/2"	73%	
Ä	67%	
#4	55%	
Total Weig	tht of Coarse Fra	action: 1125.1g
#10	42%	
#20	31%	
#40	25%	
#60	21%	
#100	17%	
#200	14.1%	
Total Weig	tht of Fine Fract	ion: 331g





Project: Downtown Kodiak MP

Work Order: D59822

ASTM D422

Lab Number 2011-1881

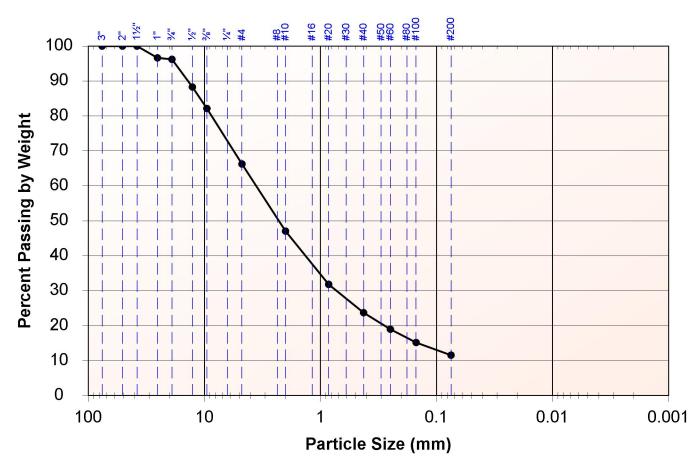
**Received** 12/4/2011

**Reported** 12/15/2011

**Location:** Test Boring 8

Sample 4 Depth 7.5'-9'

Engineering Classification: Well Graded Sand with Silt and Gravel, SW-SM



Size	Passing	Specification
3"	100%	
2"	100%	
1½"	100%	
1"	97%	
3/4"	96%	
1/2"	88%	
Ä	82%	
#4	66%	
Total Wei	ght of Coarse Fr	action: 1899.3g
#10	47%	
#20	32%	
#40	24%	
#60	19%	
#100	15%	
#200	11.5%	
Total Wei	ght of Fine Fract	ion: 301.2g





**Project:** Downtown Kodiak MP

Work Order: D59822

ASTM D422

**Lab Number** 2011-1882

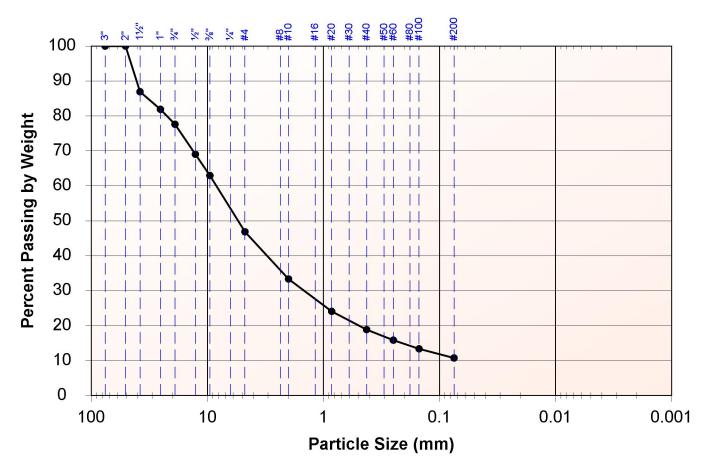
**Received** 12/4/2011

**Reported** 12/15/2011

Location: Test Boring 9

Sample 2 Depth 2.5'-4'

Engineering Classification: Poorly Graded Gravel with Silt and Sand, GP-GM



3" 100% 2" 100% 1½" 87% 1" 82% ¾" 78% ½" 69% Ä 63% #4 47%  Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%  Total Weight of Fine Fraction: 413.9g	Size	Passing	Specification
2" 100%  1½" 87%  1" 82%  ¾" 78%  ½" 69%  Ä 63%  #4 47%  Total Weight of Coarse Fraction: 1211.6g  #10 33%  #20 24%  #40 19%  #60 16%  #100 13%  #200 10.8%			Ореонновног
1½" 87%  1" 82%  ¾" 78%  ½" 69%  Ä 63%  #4 47%  Total Weight of Coarse Fraction: 1211.6g  #10 33%  #20 24%  #40 19%  #60 16%  #100 13%  #200 10.8%			
1" 82% 3/4" 78% 1/2" 69% Ä 63% #4 47%  Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%			
½" 69% Ä 63% #4 47%  Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%	1"		
Ä 63% #4 47%  Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%	3/4"	78%	
#4 47%  Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%	1/2"	69%	
Total Weight of Coarse Fraction: 1211.6g #10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%	Ä	63%	
#10 33% #20 24% #40 19% #60 16% #100 13% #200 10.8%	#4	47%	
#20 24% #40 19% #60 16% #100 13% #200 10.8%	Total Wei	ght of Coarse Fra	action: 1211.6g
#40 19% #60 16% #100 13% #200 10.8%	#10	33%	
#60 16% #100 13% #200 10.8%	#20	24%	
#100 13% #200 10.8%	#40	19%	
#200 10.8%	#60	16%	
	#100	13%	
Total Weight of Fine Fraction: 413.9g	#200	10.8%	
	Total Wei	ght of Fine Fracti	on: 413.9g